NEMA Standards Publication No. TR 1-1993 (R2000)

Transformers, Regulators and Reactors

Published by:

National Electrical Manufacturers Association 1300 North 17th Street, Suite 1847 Rosslyn, VA 22209

© Copyright 2000 by the National Electrical Manufacturers Association. All rights including translation into other languages, reserved under the Universal Copyright Convention, the Berne Convention for the Protection of Literary and Artistic Works, and the International and Pan American Copyright Conventions.

TABLE OF CONTENTS

	•	Page
PART 0	GENERAL	
	Forced-Air (FA) and Forced-Oil (FOA) Ratings	
	Performance	
	Radio Influence Voltage Levels	. 2
	Power Factor of Insulation of Oil-Immersed	
	Transformers	. 2
	Audible Sound Levels	. 2
PART 1	POWER TRANSFORMERS	. 5
PART 2	DISTRIBUTION TRANSFORMERS Design Test for Enclosure Security of Padmounted Compartmental Transformers	. 7
PART 3	SECONDARY NETWORK TRANSFORMERS	. 9
PART 4	DRY-TYPE TRANSFORMERS	. 11
PART 5	UNIT SUBSTATION TRANSFORMERS	. 13
PART 6	TERMINOLOGY	. 15
PART 7	TEST CODE	
	Voltage Levels	. 17
	Transformer Test Report	. 20
	Transformer Impulse Test Report	. 22
PART 8	TRANSMISSION AND DISTRIBUTION VOLTAGE REGULATORS	
PART 9	CURRENT-LIMITING REACTORS	
PART 10	ARC FURNACE TRANSFORMERS	. 27
PART 11	SHUNT REACTORS	
PART 12	UNDERGROUND-TYPE THREE-PHASE DISTRIBUTION TRANSFORMERS	. 31

FOREWORD

The standards appearing in this publication have been developed by the Transformer Section and have been approved for publication by the National Electrical Manufacturers Association. They are used by the electrical industry to promote production economies and to assist users in the proper selection of transformers.

The Transformer Section is working actively with the American National Standards Committee, C57, on Transformers, Regulators and Reactors, in the development, correlation and maintenance of national standards for transformers. This Committee operates under the procedures of the American National Standards Institute (ANSI).

It is the policy of the NEMA Transformer Section to remove material from the NEMA Standards Publication as it is adopted and published in the American National Standard C57 series. The NEMA Standards Publication for Transformers, Regulators and Reactors references these and other American National Standards applying to transformers, and is intended to supplement, without duplication, the American National Standards.

The NEMA Standards Publication for Transformers, Regulators and Reactors contains provision for the following:

- American National Standards adopted by reference and applicable exceptions approved by NEMA, if any.
- b. NEMA Official Standards Proposals. These are official drafts of proposed standards developed within NEMA or in cooperation with other interested organizations, for consideration by ANSI. They have a maximum life of five years, during which time they may be approved as American National Standards or adopted as NEMA Standards, or rescinded.
- c. Manufacturing Standards. These are NEMA Standards which are primarily of interest to the manufacturers of transformers and which are not yet included in an American National Standard
- d. Standards Which Are Controversial. These are NEMA Standards, on which there is a difference of opinion within Committee C57. The NEMA version will be included in the NEMA Standards Publication until such time as the differences between ANSI and NEMA are resolved.

NEMA Standards Publications are subject to periodic review and take into consideration user input. They are being revised constantly to meet changing economic conditions and technical progress. Users should secure latest editions. Proposed or recommended revisions should be submitted to:

Vice President, Engineering Department National Electrical Manufacturers Association 2101 L Street, N.W. Washington, D.C. 20037-1526

SCOPE

This publication provides a list of all ANSI C57 Standards that have been approved by NEMA. In addition it includes certain NEMA Standard test methods, test codes, properties, etc., of liquid-immersed transformers, regulators, and reactors that are not American National Standards.

PART 0 GENERAL

The following American National Standards have been approved as NEMA Standards and should be inserted in this Part 0:

ANSI/IEEE C57,12.00-1988	General Requirements for Liquid-Immersed Distribution, Power and Regulating Transformers
ANSI/IEEE C57,12.01-1989	General Requirements for Dry Type Power and Distribution Transformers
ANSI C57.12.10-1988	Requirements for Transformers 230,000 volts and below, 833/958-8333/10,417 kVA single-phase 750/862-60,000/80,000/100,000 kVA three phase, including supplements
ANSI C57.12.70-1993	Terminal Markings and Connections for Distribution and Power Transformers
ANSI/IEEE C57,12.90-1993	Test Code for Liquid-immersed Distribution, Power & Regulating Transformers and Guide for Short-Circuit Testing of Distribution & Power Transformers
ANSI/IEEE C57.19.00-1992	General Requirements and Test Procedure for Outdoor Apparatus Bushings
ANSI/IEEE C57.19.01-1992	Standard Performance Characteristics & Dimensions for Outdoor Apparatus Bushings
ANSI/IEEE C57.92-1992	Guide for Loading Mineral-oil-immersed Power Transformers up to and including 100 MVA with 55C or 65C Average Winding Rise

The NEMA Standards TR 1-0.01 through TR 1-0.09 on the following pages (see Part 0 Pages 1-9) also apply generally to transformers.

0.01 PREFERRED VOLTAGE RATINGS

Preferred system voltages and corresponding transformer voltage ratings are given in the American National Standard for Electric Power Systems and Equipment--Voltage Ratings (60 Hz), C84.1-1989. It is recommended that these ratings be used as a guide in the purchase and operation of transformers.

0.02 FORCED-AIR (FA) AND FORCED-OIL (FOA) RATINGS

Under the conditions of par. 5.11 of American National Standard ANSI/IEEE C57.12.00-1988, the relationship between self-cooled ratings and forced-air-cooled or forced-oil-cooled ratings shall be in accordance with Table 0-1.

Table 0-1
FORCED-AIR AND FORCED-OIL RATINGS RELATIONSHIPS

	Self-cooled R	atings* (kVA)		-Cooled Ratings liary Cooling
Class	Single Phase	Three Phase	First Stage	Second Stage
OA/FA	501-2499	501-2499	115	
OA/FA	2500-9999	2500-11999	125	
OA/FA	10000 and above	12000 and above	133-1/3	•-
OA/FA/FA	10000 and above	12000 and above	133-1/3	166-2/3
OA/FA/FOA	10000 and above	12000 and above	133-1/3	166-2/3
OA/FOA/FOA	10000 and above	12000 and above	133-1/3	166-2/3

^{*}In the case of multi-winding transformers or autotransformers, the ratings given are the equivalent two-winding ratings.

PERFORMANCE

0.03 RADIO INFLUENCE VOLTAGE LEVELS

The following values apply to liquid-filled transformers. They do not apply to load tap changing during switching or to operation of auxiliary relays and control switches.

0.03.1 Distribution Transformers

Radio influence voltage levels for distribution transformers, for systems rated 69 kV and less, shall not exceed 100 microvolts when measured in accordance with Section 7.01. The test voltage shall be the line-to-neutral voltage corresponding to 110 percent excitation of the transformer. This will be the coil voltage for wye connections and 1/3 times the coil voltage for delta connections.

0.04 POWER FACTOR OF INSULATION OF OIL-IMMERSED TRANSFORMERS

While the real significance which can be attached to the power factor of oil-immersed transformers is still a matter of opinion, experience has shown that power factor is helpful in assessing the probable conditions of the insulation when good judgement is used.

The proper interpretation of power factor of oil-immersed transformers is being given careful attention by manufacturers in connection with the problems of (1) selecting insulating materials, (2) sealing, and (3) processing the transformers. However, it is the comparative values which are guides for the successful solution for these problems rather than an absolute value of power factor.

The generally accepted factory tests for proving the insulation level are the prescribed low-frequency tests and impulse tests given in the American National Standard C57.12.90-1993.

When required, a factory power-factor test can be made, and this measurement will be of value for comparison with field power-factor measurements to assess the probable condition of the insulation. It is not feasible to establish standard power-factor values for oil-immersed transformers because:

- a. Experience has definitely proved that little or no relation exists between power factor and the ability of the transformer to withstand the prescribed dielectric tests.
- Experience has definitely proved that the variation in power factor with temperature is substantial and erratic so that no single correction curve will fit all cases.

When a factory power-factor measurement of a transformer is required, the measurement should be made with the insulation at room temperature, preferably at or close to 20°C.

0.05 AUDIBLE SOUND LEVELS

Transformers shall be so designed that the average sound level will not exceed the values given in Tables 0-2 through 0-4 when measured at the factory in accordance with the conditions outlined in ANSI/IEEE C57.12.90-1993.

The guaranteed sound levels should continue to be per Tables 0-2 through 0-4 until such time as enough data on measured noise power levels becomes available.

Sound pressure levels are established and published in this document. Sound power may be calculated from sound pressure, using the method described in C57,12.90-1993.

Rectifier, railway, furnace, grounding, mobile and mobile unit substation transformers are not covered by the tables. The tables do not apply during the time that power switches are operating in load-tap-changing transformers and in transformers with integral power switches.

ble 0-2
-IMMERSED POWER TRANSFORMERS

AUDIBLE SOUND LEVELS FI

Column 1 - Cleas*OA, Ow and FOW Raings
Column 2 - Cleas* FA and FOA First stage Auxiliary Cooling***
Column 3 - Straight FOA* Ratings, FA*FOA* Second-stage Auxiliary Cooling**

Column 3 - Straight FOA* Ratings, FA*FOA* Second-stage Auxiliary Cooling**

The content of the cooling of the cool

Average Sound								Equiv	Equivalen Two-winding Rating&	Ing Reting								
Level 11.	"	350 kV Bit, and Below	Below	•	450, 650, 850 kV BK.	/ B.K.	75	750 and 625 kV BR	ِ اِ	4008	900 and 1050 kV Bit.	-	-	1176 KV BR			1300 kV Bit, and Above	*
Decibels	-	~	en	-	~	_	-	2	6	_	2	•	-	~	٠	-	~	
57	8	ı	:	ì	i	·	ŧ	:	:	:	i	1	÷	:	ī	;	i	Ē
38	00 <u>0</u>		:	i		:	:	:	į	1	•	•	:	ŗ	:	1	:	i
28	1	:	ł	ě	;	ł	ŧ	į	i	Ē	:	:	ŗ	:	ł	ì	ı	:
8	1500	:		0001	į	ī	:	:	;	;	į	i	1	:	i	:		ł
5	2000		:	:	ŧ		:	i		i	:	ı	ŧ	:	:	i	ŧ	ŀ
2	2500	ì	:	<u>8</u>	;			:			ı	ŧ	i	:		ı	:	ŧ
\$	3000	ł	:	2002	•	٠	:	i	Ŧ	:	;	:	;	:	£	ı	ŧ	ŀ
3	4000	;	ŧ	200	1	:	ı	i	i	į	ī	1	:	ì	1	;	:	i
*	2000	ı	?	3000	i	;	ı	ï	;	•	į	:	1	ı	٠,	:	ī	i
*	900	:	:	Q			3000	:	:	ŧ	i	ŧ	į	:	;	f	ŧ	Ī
67	7500	82504A	r	9006	3750AA		4000	312544		:	:	:	<u>:</u>	ı	į	î	:	•
. 5	10000	7500		9009	900		2000	3750	:	:	;	:	;	:	;	!	:	1
2	12500	8375		7500	6250		900	2000	;	:	;	í	ŧ	i	:	:	:	i
2	00051	0550		10000	2500		7500	6250	;	;	i	i	:	:	í	ŧ	:	ŧ
2;			•	13600	4224		00001	7500	:	;	i	:	i	;	:	;	;	i
=	2000	8		200	ì				!	i	i							
\$	96000	30000	20900	000	12500	,	12500	9375	:	1	:	ì	;	:	÷	i	;	i
٠,	2000	76607	3600	2000	16067		00051	12500	;	12500	î	:	ì	:		Ē	;	:
2		10007	200		10001		į	18667	!	00091	: :	. ;	12500		•	;	1	i
×		202		4364	200	2000		0000	2000	20000	16467		15000	: :		12500		i
2	30000	4000	Por e		10007	2000		2000		3600		- Computer	20000	16ct7	: :	15000		
*	0000	23030	90000	40000	33533	2555	200	19092							:		Ŀ	i
			2000	******	******	7.00	4000	mm	200	30000	24467	25000		00000	20800	2000	19667	
		200	1000		2000			4000	41007	4000	2002	24720	30000	24667	25000	25000		20800
8 2	10000	200	2000	9000		2000		6000		20009	40000	41687		13313	33333	30000	20057	00052
2	:	1000		-	10000			2000			61131	2000		40000	41667	40000		11333
8	1	13333	13333	10000	2000	7577	2	10000	Ì					19333	9000	1		41647
.	E	ŗ	100067	i	106667	100000	20000	W.Y.	2002		200	7000		2				
			***************************************		******	******		100467	100000	10000	90008	60333	9000	1999	29999	90000	\$3303	00005
2	ŧ	E	-	i	20000		:		1 400000		10447	00000		0000	Breeze	BOOOD	10000	599637
2	:	:	20000	:	ì	100001	į	2	10000	:	12322	******		(Need)	10000	COLOR	BOOM	222
Z	:	ī	30000	:	i	ZONO	į	ì	10000	ı		10000			,,,,,,,,		Cadde?	10000
2	1	ŧ	400000	E	i	250000	ţ	:	2000	i	;	10000/				Ī	1	
*	ì	ŧ	i	:	1	300000	i	1		ŧ	i	2000	Ŧ	į	3	:	-	
						,			-			260000			2000000	i	:	100667
-	ŧ	ŧ	ŧ	:	i		1	ŧ		!	i		ţ	ı	250000	l		50000
2	ŧ	1	ł	ŧ	:	ł	:	i		:	i	40000	ì		00000	:	ı	250000
2	i	:	i	;	ŧ	1	ŧ	:	į	į	£		:		70007	ì		20000
8	i	i	i	ī	;		ŧ	:	i	•	÷	:	į			í	ŧ	
=	:	;	į	į	ì	ĭ	ŧ	:	ŧ	i	!	ŧ	•	i	ŧ	:	1	
		1	Nonel Standard	4 CS7 12 An 1084														

*Classes of cooking (see 2.6.1 of American National Standard C57.12.00-1988.

*First: and second stage sunitisty cooking (see TR 10.00).

†For column 2 and 3 ratings, the sound levels are with the sunitisty cooking equipment in operation.

††For intermediate kVA ratings, use the average sound level of the next larger kVA rating.

4.The equivalent kno-whiding 55 °C or 65 °C rating is defined as one half the sum of the kVA rating of all windings.

4.A.S.Inty-seven decibels for all XVA ratings equal to this or smalter.

Table 0-3

AUDIBLE SOUND LEVELS FOR LIQUID-IMMERSED

DISTRIBUTION TRANSFORMERS AND NETWORK TRANSFORMERS

Equivalent Two-winding kVA	Average Sound Level, Decibels
0–50	48
51–100	51
101–300	55
301-500	56
750	57
1000	58
1500	60
2000	61
2500	62

Table 0-4
AUDIBLE SOUND LEVELS FOR DRY-TYPE TRANSFORMERS 15000-VOLT
NOMINAL SYSTEM VOLTAGE AND BELOW

Equivalent	Average Sound	Level, Decibels	Equivalent	Average Sound Level, Decibels
Two-Winding kVA	Self-cooled Ventilated*	Self-cooled Scaled*	Two-winding	Ventüsted Forced Air Cooled **,1
0-50	50	50	***	***
51-150	55	55	•••	4.4
151-300	58	57	3-300	67
301-500	60	59	301-500	67
501700	62	61	501-833	67
701-1000	64	63	834-1167	67
1001-1500	65	64	1168-1667	68
1501-2000	66	65	1668-2000	69
2001-3000	68	66	2001-3333	71
3001-4000	70	68	3334-5000	73
4001-5000	71	69	5001-6667	74
5001-6000	72	70	6668-8333	75
6001-7500	73	71	8334-10000	76

^{*} Class AA rating

^{**}Does not apply to sealed-type transformers

[†]Class FA and AFA ratings

Part 1 POWER TRANSFORMERS

The American National Standard C57.12.10-1988 has been approved as a NEMA Standard for power transformers and should be inserted in this Part 1.

The ANSI/IEEE Standard C57.92-1992, has been approved by NEMA and should be inserted in this Part 1.

The following other parts of this NEMA Publication No. TR 1 shall also apply:

- a. Part 1 General
- b. Part 6 Terminology
- c. Part 7 Test Code
- d. Part 12 Underground-Type Three-Phase Distribution Transformer

Part 2 DISTRIBUTION TRANSFORMERS

The following American National Standards have been approved as NEMA Standards for distribution transformers and should be inserted in this Part 2:

	·
ANSI C57.12.20-1988	Requirements for Overhead-Type Distribution Transformers, 500 kVA and Smaller: High Voltage, 34500 Volts and Below; Low Voltage, 7970/13800Y Volts and Below
ANSI C57,12,21-1980	Requirements for Pad-Mounted, Compartmental-Type, Self-Cooled, Single-Phase Distribution Transformers with High-Voltage Bushings; (High-Voltage, 34500 Grd Y/19920 Volts and Below; Low-Voltage, 240/120 Volts; 167 kVA and Smaller)
ANSI C57.12.22-1989	Requirements for Pad-Mounted, Compartmental-Type, Self-Cooled, Three-Phase Distribution Transformers with High-Voltage Bushings 2500 kVA and Smaller; High-Voltage, 34500 Grd Y/19920 Volts and Below; Low Voltage, 480 Volts and Below
ANSI C57.12.23-1992	Requirements for Underground-Type Self-Cooled Single-Phase Distribution Transformers, with Separable Insulated High-Voltage Connectors; High-Voltage 24940 Grd Y/14400 Volts and Below; Low-Voltage 240/120; 167 kVA and Smaller
ANSI C57.12.25-1990	Requirements for Pad-Mounted, Compartmental-Type, Self-Cooled, Single-Phase Distribution Transformers with Separable Insulated High-Voltage Connectors: High-Voltage 34500 Grd Y/19920 Volts and below: Low-Voltage 240/120 Volts; 167 kVA and Smaller
ANSI C57.12.26-1987	Pad-Mounted Compartmental-Type Self-Cooled, Three-Phase Distribution Transformers for use with Separable High-Voltage Connectors (High-Voltage 34500 Grd Y/19920 Volts and Below: 2500 kVA and Smaller)
ANSI C57.91-1992	Guide for Loading Mineral Oil-Immersed Overhead-type Distribution Transformers with 55C or 65C Average Winding Rise

The following parts of this NEMA Publication No. TR 1 shall apply for distribution transformers:

Part 0 General

Part 6 Terminology

Part 7 Test Code

Part 12 Underground-type Three-Phase Distribution Transformers

2.01 DESIGN TEST FOR ENCLOSURE SECURITY OF PADMOUNTED COMPARTMENTAL TRANSFORMERS

This standard provides a means for evaluating the security of enclosures for transformers conforming to the following American National Standards.

ANSI C57.12.21-1980	Requirements for Pad-Mounted, Compartmental-Type, Self-Cooled, Single-Phase Distribution Transformers with High-Voltage Bushings; High-Voltage, 34500 Grd Y/19920 Volts and Below; Low-Voltage, 240/120 Volts; 167 kVA and Smaller
ANSI C57.12.22-1989	Requirements for Pad-Mounted, Compartmental-Type, Self-Cooled, Three-Phase Distribution Transformers with High-Voltage Bushings 2500 kVA and smaller; High-Voltage, 34500 Grd Y119920 Volts and Below; Low Voltage 480 Volts and Below
ANSI C57.12.25-1990	Requirements for Pad-Mounted, Compartmental-Type, Self-Cooled, Single-Phase Distribution Transformers with Separable Insulated High-Voltage Connectors: High-Voltage 34500 Grd Y/19920 Volts and below: Low-Voltage 240/120 Volts; 167 kVA and Smaller

Previous page is blank.

ANSI C57.12.26-1987 Pad-Mounted Compartmental-Type Self-Cooled, Three-Phase Distribution Transformers for use with Separable High-Voltage Connectors (High-Voltage 34500 Grd Y/19920 Volts and Below: 2500 kVA and Smaller)

Part 3 SECONDARY NETWORK TRANSFORMERS

The American National Standard Requirements for Secondary Network Transformers, Subway and Vault Types (Liquid Immersed), C57.12.40-1990, (with the exception of paragraphs 5.5.4 and 11.5.2 on finishes) have been approved as NEMA Standards for secondary network transformers and should be inserted in this Part 3.

The following other parts of this NEMA Publication No. TR 1 shall also apply for secondary network transformers:

a. Part 0 General

b. Part 6 Terminology

c. Part 7 Test Code

Part 4 DRY-TYPE TRANSFORMERS

The following American National Standards have been approved as NEMA Standards for dry-type transformers and should be inserted in this Part 4:

ANSI/IEEE C57.12.01-1989	General Requirements for Dry-type Distribution and Power Transformers
ANSI/IEEE C57.12.91-1979	Test Code for Dry-Type Distribution and Power Transformers
ANSI C57.12.50-1989	Requirements for Ventilated Dry-Type Distribution Transformers, 1 to 500 kVA, Single-Phase; and 15 to 500 kVA, Three-Phase; With High-Voltage 601-34500 Volts, Low-Voltage 120-600 Volts
ANSI C57.12.51-1989	Requirements for Ventilated Dry-Type Power Transformers, 501 kVA and Larger, Three-Phase With High-Voltage 601-34500 Volts, Low-Voltage 208Y/120-4160 Volts
ANSI C57.12.52-1989	Requirements for Sealed Dry-Type Power Transformers, 501 kVA and Larger, Three-Phase, With High-Voltage 601-34500 Volts, Low-Voltage 208Y/120-4160 Volts
ANSI/IEEE C57.94-1982	Recommended Practices for Installation, Application, Operation and Maintenance of Dry-Type General Purpose Distribution and Power Transformers
ANSI/IEEE C57.96-1989	Guide for Loading Dry-Type Transformers, Appendix to C57.12 Standards

Part 5 **UNIT SUBSTATION TRANSFORMERS**

The following other parts of this NEMA Publication No. TR 1 shall also apply for unit substation transformers.

a. Part 0 General

- b. Part 6 Terminology
- c. Part 7 Test Code

Previous	page	is	blank.
----------	------	----	--------

Part 6 TERMINOLOGY

The ANSI/IEEE Standard C57.12.80-1992, has been approved as a NEMA Standard for terminology and should be inserted in this Part 6.

Previous page is blank.

Part 7 TEST CODE

The American National Standard ANSI/IEEE C57.12.90-1987, has been approved as a NEMA Standard for transformer tests and should be inserted in this Part 7.

This NEMA standard, Part 7, shall also apply for transformer tests.

The ANSI/IEEE Standard C57.98-1992, should be inserted in this Part 7.

7.01 TEST CODE FOR MEASUREMENT OF RADIO INFLUENCE VOLTAGE LEVELS

a. Apparatus

The apparatus to be tested under this code can be divided into two general classes as follows:

- Class 1— Potential-type transformer apparatus, such as transformers for step-up, step-down or interconnected service, and some arrangements of regulating transformers and autotransformers.
- Class 2— Series-type transformer apparatus, such as series transformers, shunt (iron core) reactors, current-limiting reactors and some arrangements of regulating transformers and auto-transformers.

b. Equipment

The equipment and general method used in determining the radio influence voltage shall be in accordance with the NEMA Standards Publication Methods of Measurement of Radio Influence Voltage (RIV) of High-voltage Apparatus, 107-1964 (R-1971, 1976, R-1992). For an alternate method, see par. E, Use of Bushing Capacitance Tap.

c. Connections for testing—Class A-1 Apparatus
The test voltage shall preferably be impressed
across the winding under test (see Fig. 7-1). It
may, however, be induced from a winding other
than that being tested (see Fig. 7-2). In order
that the results be comparable, the circuit arrangements and constants must be as shown in
Fig. 7-1 or 7-2. The winding shall be tested first
with one end grounded and then with the other
end grounded.

The test on a reduced-voltage neutral terminal shall correspond to the insulation class of the neutral. Windings with one end solidly grounded obviously will receive no test on the grounded end.

One terminal of each winding not under test, the ground terminal if one is available, shall be connected to the tank and ground.

- d. Connections for testing—Class A-2 Apparatus The test voltage shall be applied to the winding under test, with all terminals of the winding under test tied together (see Fig. 7-3).
- e. Use of bushing capacitance tap

If radio influence voltage is measured at the capacitance tap of the bushing, a suitable device shall be used which can be tuned with the bushing tap to ground capacitance at the measuring frequency. This device shall constitute all circuit elements from the capacitance tap of the bushing to the radio noise meter.

The coaxial cable, an element of the device, may be any suitable impedance and need not be terminated in its characteristic impedance. The purpose of the device is to minimize the dividing effect of the bushing capacitance and to convey the radio influence voltage to the radio noise meter with minimum attenuation. See Fig. 7-4 and 7-5.

 Calibration for circuits using bushing capacitance tap

The calibration ratio will be determined by:

- Applying to the terminal under test the output of a sine-wave signal generator at approximately 100 microvolts and at the measuring frequency, or that of a pulse signal generator at approximately 100 microvolts.
- Measuring the voltage on the terminal with the radio noise meter connected directly to the terminal.
- Measuring, with the same radio noise meter, the voltage appearing in the test circuit at the location where the radio noise meter will be connected during the radio influence voltage measurement on the transformer (a second radio noise meter shall be permitted to be used instead, provided its relationship to the first radio noise meter has been established).
- It shall be established that this calibration ratio remains valid over the radio influence voltage range of interest.

The ratio of the voltage measured with the radio noise meter at the terminal to the voltage measured with the radio noise meter at the normal location in the circuit which has been selected for the corona test on the transformer will be applied as a correction factor to the radio influence voltage reading obtained during the corona test to determine the actual radio influence voltage at the terminal of the winding under test.

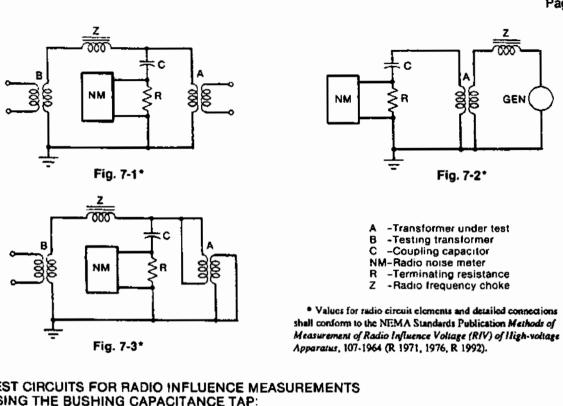
g. Test voltage

The test voltage shall be determined from the preferred nominal system voltage in accordance with 0.04 in Part 0, except that the test voltage shall not exceed 110 percent of the rated voltage of the winding on the highest tap connection.

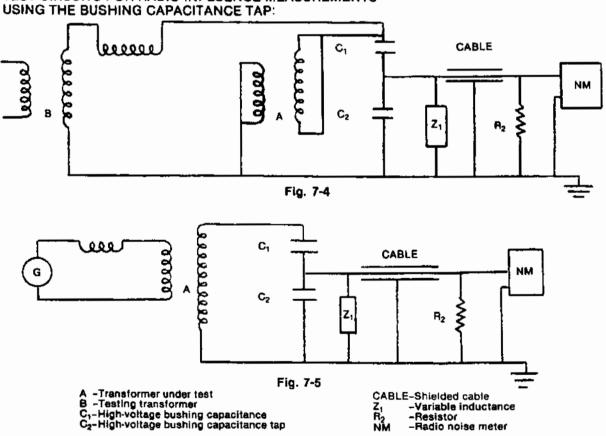
h. Precautions in making tests

The following precautions should be observed in measuring the radio influence voltage. The apparatus should be:

- Tested at approximately the same temperature as the room in which the tests are made
- Located as to provide the outside clearances recommended.



TEST CIRCUITS FOR RADIO INFLUENCE MEASUREMENTS



7.02 TRANSFORMER TEST REPORT

To facilita	te safe and effective operation of transformers it is recommended that the following information be included
in the test re	port:

	1621				Purc	haser's	Order I	No	N	lfr.'s R ef .	No				
								rtz							
Vindin	9 (1) _				kVA	(2)			k'	VA ⁽³⁾ _					kVA
eps_	<u> </u>														
nd re	gulation	EXCITING are based as in series	on watti	NT, LO meter	OSSE r mea	S AND	IMPED ents. Fo	ANCE—Base or three-phase	d on nors transfo	mal rating rmers the	unless resista	other nces	rwise given	stated. are the	Los sum
		Resi	stance (n Ohr	ms			<u> </u>	Watts	Loss and I	Impedan	ce at	85°C		
Serial No.			at 85°	С		Exciting Current Percent	No Load	to	v	to		<u>۷</u>			_v
Serial No.	m	(2)	(2)	(3)	#1 100%	in Watts 100%		kVA			kVA			 kV	
		- '''	(2)	+	3)	Voltage	Voltage	Load Loss	%Imp.	Load Lo	088 %	lmp.	LORG	Loss	- MIN
				T	一				 			-			
Au		-	\vdash	╄				Total Loss	 	Total Lo	388	_	Total	Loss	
Avera			┿	╄	-			 			+	-			
rial N	10	RISES are								windings o					
rial Nulti-w ot be all be at the	inding to the same on sep- e fluid ter Temp. Rise Guar.	ransformer e as that f arate lines mperature Fluid Losses	heat ru or the n In the T rise and	n cor naxim empe wind • Amb	nnect num eratur ling ri b.	tions fo losses re Rise ises en	or the d which p table o tered or	letermination produce the m of the Test Re of a common line Winding Di and Winding	of the maximum port Forme correction	naximum fluid rise n. Precau spond to t Above Av Shorted W	winding Such utions s the same verage Fi	rise: tem; hould test	s over peratu d be ta condi	ambie re rise aken to klions. by Res.	ent m entri assu
erial Nulti-woot be hall be at the	inding to the same on sepa e fluid ter Temp.	ransformer e as that f arate lines mperature Fluid	heat ru or the n In the T rise and	n cor naxim empe wind	nnect num l eratur ling ri b.	tions fo losses re Rise ises en	or the d which p table o tered or	letermination produce the m of the Test Re of a common line Winding Di and Winding	of the maximum port Forme correction	naximum fluid rise n. Precai spond to t	winding s. Such utions s the same verage Fi	rise: tem; hould test	s over peratu d be ta condi	ambie re rise aken to tions.	ent m entri assu
erial Nulti-woot be hall be hall be hall be	inding to the same on sep- e fluid ter Temp. Rise Guar.	ransformer e as that f arate lines mperature Fluid Losses	heat ru or the n In the T rise and	n cor naxim empe wind • Amb	nnect num eratur ling ri b.	tions fo losses re Rise ises en	or the d which p table o tered or	letermination produce the m of the Test Re of a common line Winding Di and Winding	of the maximum port Forme correction	naximum fluid rise n. Precau spond to t Above Av Shorted W	winding Such utions s the same verage Fi	rise: tem; hould test	s over peratu d be ta condi	ambie re rise aken to klions. by Res.	ent m entri assu
erial Nulti-woot be hall be hall be hall be	inding to the same on sep- e fluid ter Temp. Rise Guar.	ransformer e as that f arate lines mperature Fluid Losses	heat ru or the n In the T rise and	n cor naxim empe wind • Amb	nnect num eratur ling ri b.	tions fo losses re Rise ises en	or the d which p table o tered or	letermination produce the m of the Test Re of a common line Winding Di and Winding	of the maximum port Forme correction	naximum fluid rise n. Precau spond to t Above Av Shorted W	winding Such utions s the same verage Fi	rise: tem; hould test	s over peratu d be ta condi	ambie re rise aken to klions. by Res.	ent m entri assu
erial Nulti-wolt be hall be ha	inding to the sam e on sep- e fluid ter Temp. Rise Guar.	ransformer e as that f arate lines mperature Fluid Losses Dissipate	heat ru or the n in the T rise and R. Abov	n cornaxim empe wind Amb	nnect num eratur ling ri b.	tions to losses re Rise ses en	or the d which p table o tered or Energiz	letermination produce the m of the Test Re n a common li Winding Di red Winding kV Amps	of the naximum port Forme correctifferentia	naximum fluid rise n. Precal spond to t Above Av Shorled W Tap-kV	winding Buch utions s the same verage F Winding	rise: tem; hould test luid	s over peratu d be ta condi	ambie re rise aken to klions. by Res.	ent m entri assu
erial Nulti-work be hall be ha	inding to the sam e on sep- e fluid ter Temp. Rise Guar.	ransformer e as that f arate lines mperature Fluid Losses Dissipate	heat ru or the n in the T rise and R. Abov	n cornaxim empe wind Amb	nnect num eratur ling ri b.	tions to losses re Rise ses en	or the d which p table o tered or Energiz Tap-i	letermination produce the month of the Test Remains a common like Winding Direct Winding RV Amps	of the naximum port For he correct ifferential	naximum fluid rise m. Precai spond to t Above Av Shorted W Tap-kV	winding Such utions s the same verage F Vinding Amps	rise: tem; hould test luid	s over peratu d be ta condi Rise i	ambie re rise aken to (tions.	ent m entri assu
erial N ulti-wot be nell but at the	inding to the same on september of the same on september of the same on september of the same of the s	ransformer e as that f arate lines mperature Fluid Losses Dissipate	heat ru or the n in the T rise and R. Above	n connaximemper wind	nnect num eratur ling ri b. Ave	tions to	or the d which p table o tered or Energiz Tap-l	letermination produce the m of the Test Re n a common li Winding Di red Winding kV Amps	of the maximum port Forme correct ifferential	naximum fluid rise n. Precal spond to t Above Av Shorled W Tap-kV	winding Buch utions s the same rerage F Winding Amps	rise: tem; hould test luid	s overperatud be tale condition (1)	ambie re rise aken to klions. by Res.	*C (3)
erial Nulti-wot be hall be hal	inding to the same on september of september of the same on september of the same of the s	ransformer e as that f arate lines mperature Fluid Losses Dissipate	heat ru or the n in the T ise and R. Above	n connaximemper wind	nnectinum eratur ing ri b. Ave	tions to losses re Rise ses en	or the d which p table o tered or Energiz Tap-l	letermination produce the margin the Test Re na common li Winding Dired Winding kV Amps	of the maximum port Forme correct ifferential	naximum fluid rise m. Preca ipond to t Above Av Shorted W Tap-kV	winding Buch utions s the same rerage F Winding Amps	rise: tem; hould test luid	s overperatud be tale condition (1)	ambiere rise sken to klons. (2)	*C (3)
rial Nulti-walt be all	inding to the same on september of the same on september of the same on september of the same of the s	ransformer e as that f arate lines mperature Fluid Losses Dissipate STS—If im PPLIED POT plied betwa ings connect	heat ru or the n in the T rise and R. Above Dulse Te ENTIAL en each tied to c	n cornaxim empewind • Ami Fop *C	nnection in the rection in the recti	quired,	or the d which p table o tered or Energiz Tap-l	letermination produce the margin the Test Re na common li Winding Dired Winding kV Amps	of the maximum port Forme correct ifferential former Imp	naximum fluid rise m. Preca ipond to t Above Av Shorted W Tap-kV	winding Such utions si the same rerage F Winding Amps Fileport	rise: tem; hould e test luid	s overperatude to be tall to be t	ambiere rise sken to klons. (2) ion of T Second	ent m entri assu *C (3)
erial Nulti-work be all builti-work be all builti-work be all builti-work be all builti-work builti-wo	inding to the same on september of the same on september of the same on september of the same of the s	ransformer e as that f arate lines mperature Fluid Losses Dissipate STS—If im PPLIED POT plied betwa ings connec	heat ru or the n in the T rise and R. Above Dulse Te ENTIAL en sach tied to c	n cornaxim empo wind Amil Top *C	nnectinum eraturiling ri b. Ave *CC	quired,	or the d which p table o tered or Energiz Tap-I	letermination produce the margin the Test Re na common li Winding Dired Winding kV Amps	of the maximum port Forme correct ifferential former Imp	naximum fluid rise m. Preca ipond to t Above Av Shorted W Tap-kV	winding Such utions si the same rerage F Winding Amps Fileport. Itage ed	rises temp hould be test	s overperatud be tale condition (1) Rise (1) Duration 5	ambiere rise aken to kions. (2) ion of T Second	entri mentri assu
erial Nulti-work be all by at the Cool lode	rinding to the same on sep- official from the same on sep- official from the following of the same of	ransformer e as that f arate lines mperature Fluid Losses Dissipate STS—If im PPLIED POT plied betwa ings connec	heat ru or the n in the T rise and R. Above Dulse Te ENTIAL en sach tied to c	n cornaxim empo wind Amil Top *C	nnectinum eraturiling ri b. Ave *CC	quired,	or the d which p table o tered or Energiz Tap-I	letermination produce the margin the Test Re na common li Winding Dired Winding kV Amps	of the maximum port Forme correct ifferential former Imp	naximum fluid risem. Precai pond to t l Above Av Shorled W Tap-kV L Tap-kV	winding Such utions si the same rerage F Winding Amps Fileport. Itage ed	rises temp hould be test	s overperatud be tale condition (1) Rise (1) Duration 5	ambiere rise aken to kions. (2) ion of T Second	entri mentri assu
erial N ulti-wot be hall be ha	inding to the same on seperature of the same on seperature of the same on seperature of the same of th	ransformer e as that f arate lines mperature Fluid Losses Dissipate STS—If Im PPLIED POT plied betwa ings connect OTENTIAL S	heat ru or the n in the T rise and R. Above ad culse Te ENTIAL en sach tied to c	n cornaxim empowind wind wind of a mests a TEST wind or a mests a mes	nnectinum eraturiling ri b. Ave +C	quired,	or the d which p table o tered or Energia Tap-l see sep	letermination produce the margin the Test Re na common li Winding Dired Winding kV Amps	of the naximum port Forme correct ifferential former important imp	naximum fluid rise m. Precal spond to	winding Such utions s the same verage F Winding Amps Amps Amps Amps Amps Amps	rises temphould be test full distributed by test full distributed by the t	S overperatural be tall conditions (1) Duration terminates terminates terminates (2)	ambiere rise aken to kions. by Res. (2) ion of 1 Second	ent m entri assu

chaser Purchaser's Order No Mir.'s References							
					insulating Fluid		
vinding		Volts	X-winding				Volt
Serial No.	Osciliograms	Test*	Surge Applied on Terminal No.	kV Required	kV Applied	Microsecond to Crest	Microsecond to Flashover
	uced Full Wave		•cw-	Chopped Wave			*FW-Full Wa

_ Pages

7.04 REACTOR TEST REPORT

To facilitate safe and effective operation of transformers it is recommended that the following information be included
the test report:

Purchaser Date of Tests			
Type			
Type	No		
For connection in			
RESISTANCES, LOSSES AND IMPEDANCE are based on normal rating, unless otherwise swattmeter measurements. Resistance at 85°C			
Average Guarantee TEMPERATURE RISE In degrees C corrected to instant of shutdown.	tated. Losses are based on		
Phase A Phase B Phase C Walts 85 °C Average Guarantee TEMPERATURE RISE In degrees C corrected to instant of shutdown.	Impedance		
TEMPERATURE RISE In degrees C corrected to instant of shutdown.	Volts %		
TEMPERATURE RISE In degrees C corrected to instant of shutdown.			
TEMPERATURE RISE In degrees C corrected to instant of shutdown.			
TEMPERATURE RISE In degrees C corrected to instant of shutdown.			
TEMPERATURE RISE In degrees C corrected to instant of shutdown.	 _		
TEMPERATURE RISE In degrees C corrected to instant of shutdown.			
TEMPERATURE RISE In degrees C corrected to instant of shutdown.			
TEMPERATURE RISE in degrees C corrected to instant of shutdown.			
Serial No. Ampères Rise by Resistance			
	Guarantee		
	<u> </u>		
NSULATION TESTS—high-potential tests were made on each reactor. Voltage was applied is and between phases of a polyphase reactor. Voltage at high frequency was induced in each turn strength.	between winding and ground winding to test the turn-to-		
	Induced Voltage at High Frequency		
The state of the s	radamo,		
			
			
REMARKS:			
Signed Date Approved			
Signed Date Approved	"		

Part 8 TRANSMISSION AND DISTRIBUTION VOLTAGE REGULATORS

The ANSI/IEEE Standard C57.15-1992, has been approved as NEMA Standards for transmission and distribution voltage regulators and should be inserted in this Part 8.

The ANSI/IEEE Stanard C57.95-1992. Appendix to C57.15, has been approved as NEMA Standard for Transmission and distribution voltage regulators and should be inserted in this Part 8.

Part 9 CURRENT-LIMITING REACTORS

[To Be Published]

Part 10 **ARC FURNACE TRANSFORMERS**

The following other parts of this NEMA Publication No. TR 1 shall also apply for arc furnace transformers:

a. Part 0 General

- b. Part 6 Terminology
- c. Part 7 Test Code

Previous page is blank.

Part 11 SHUNT REACTORS

The American National Standard, C57.21-1991, has been approved by NEMA and should be inserted in this Part 11.



NATIONAL ELECTRICAL MANUFACTURERS ASSOCIATION • 1360 NORTH 174H SARTELT • SUITE 1847 • ROSSIAN, AA 222209